## APPENDIX F

## AXIAL LOAD WITH BIAXIAL BENDING - EXAMPLE

F-1. In accordance with paragraph 4-5, design an 18- by 18-inch reinforced concrete column for the following conditions:

 $f_c' = 3,000 \text{ psi}$ 

 $f_{v} = 60,000 \text{ psi}$ 

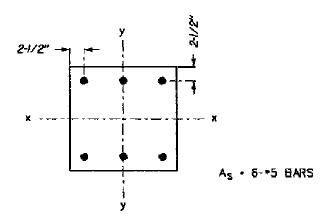
 $P_{\rm u}$  = 100 kips,  $P_{\rm n}$  =  $P_{\rm u}/0.7$  = 142.9 kips

 $M_{\rm ux}$  = 94 ft-kips,  $M_{\rm nx}$  =  $M_{\rm ux}/0.7$  = 134.3 ft-kips

 $M_{\rm uv}$  = 30 ft-kips,  $M_{\rm nv}$  =  $M_{\rm uv}/0.7$  = 42.8 ft-kips

Let concrete cover plus one-half a bar diameter equal 2.5 in.

F-2. Using uniaxial design procedures (Appendix E), select reinforcement for  $P_{\rm n}$  and bending about the x-axis since  $M_{\rm nx} > M_{\rm ny}$ . The resulting cross-section is given below.



F-3. Figures F-1 and F-2 present the nominal strength interaction diagrams about x and y axes. It is seen from Figure F-2 that the member is adequate for uniaxial bending about the y-axis with  $P_{\rm n}$  = 142.9 kips and  $M_{\rm ny}$  = 42.8 ft-kips. From Figures F-1 and F-2 at  $P_{\rm n}$  = 142.9 kips:

 $M_{\rm ox}$  = 146.1 ft-kips

 $M_{ov}$  = 145.9 ft-kips

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For a square column, must satisfy:

$$(M_{\rm nx}/M_{\rm ox})^{1.75} + (M_{\rm ny}/M_{\rm oy})^{1.75} \le 1.0$$
  
 $(134.3/146.1)^{1.75} + (42.8/145.9)^{1.75} = 0.98 < 1.0$ 

If a value greater than 1.0 is obtained, increase reinforcement and/or increase member dimensions.

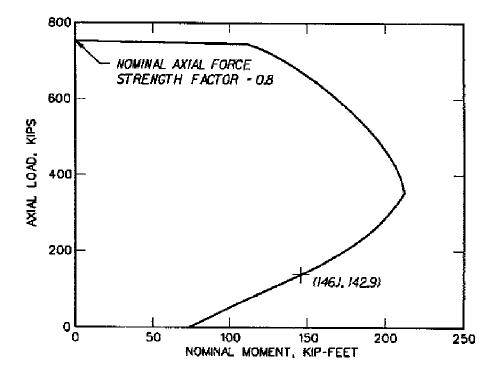


Figure F-1. Nominal strength about the X-axis

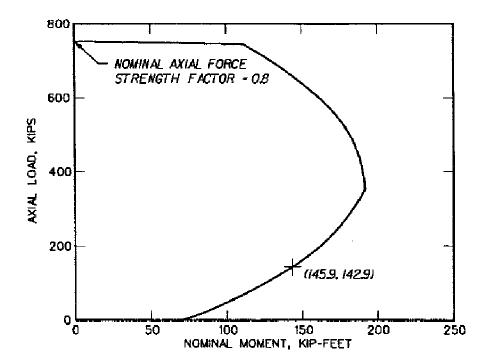


Figure F-2. Nominal strength about the Y-axis